

Hurricane Surge Response Functions



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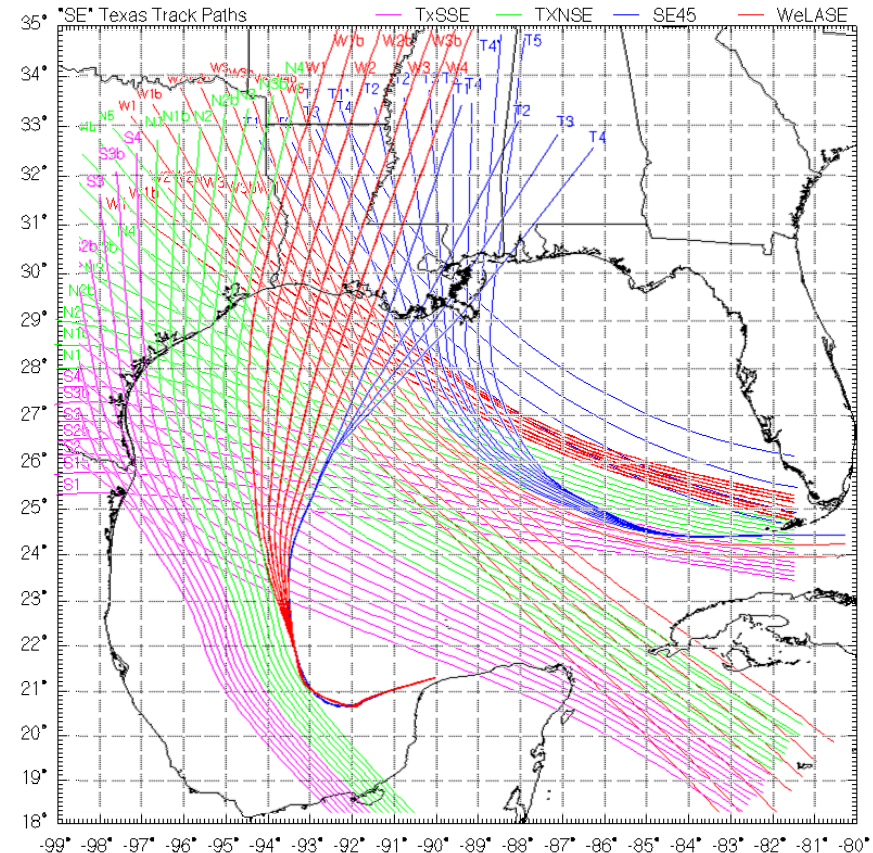
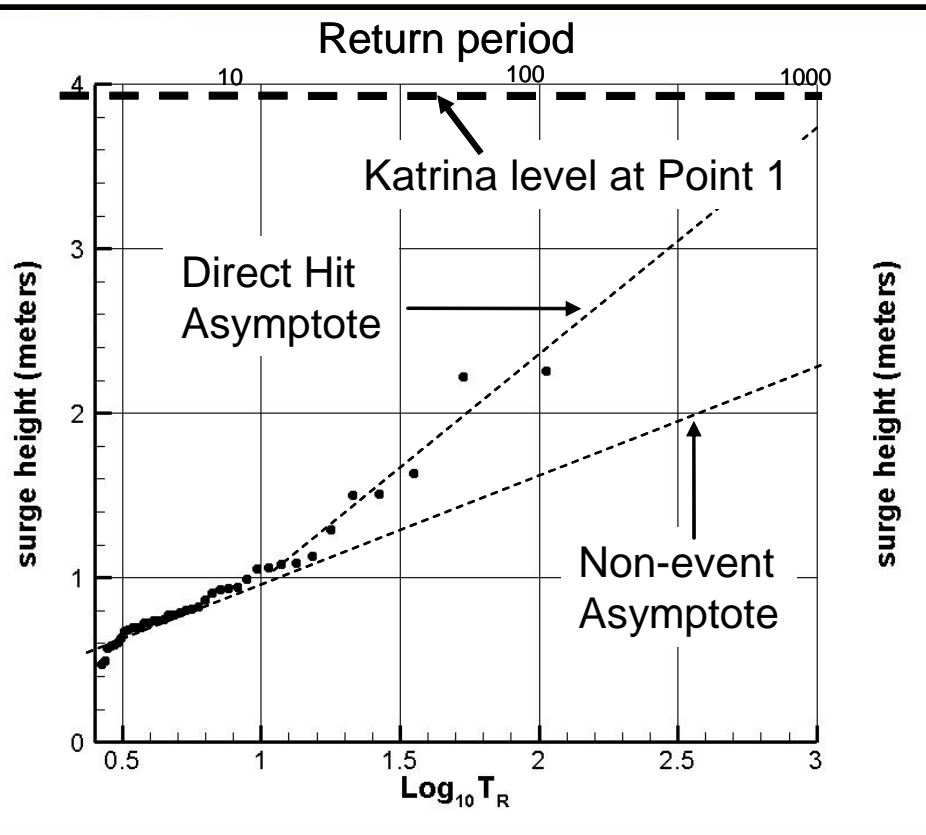
Surge Response Functions Outline

- Motivation
- Background
- Methodology
- Surge Characteristics
- Parameterization
- Results
- Ongoing Research
- Hurricane Ike Verification
- Summary



Surge Response Functions Motivation

1. An improved, efficient, and accurate risk-assessment method for coastal flooding is required.
2. Develop a continuous surge estimator for emergency response

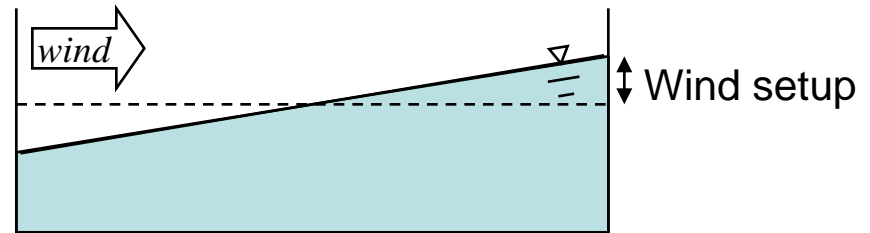


Surge Response Functions

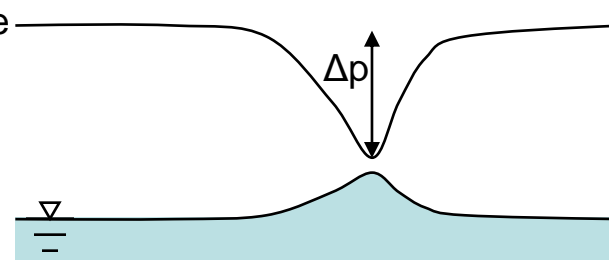
Background – Surge Generation

Primary mechanisms:

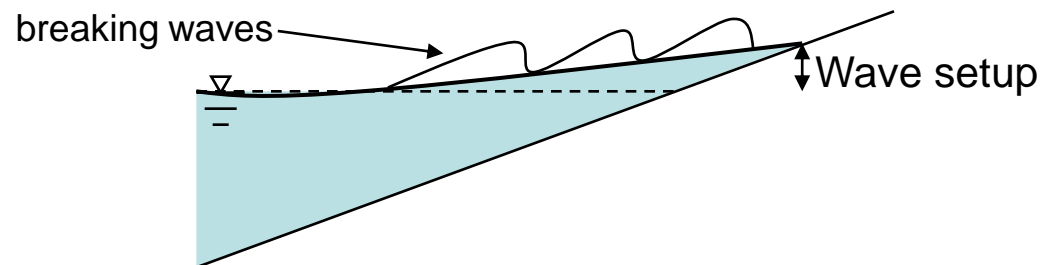
- Wind setup:



- Low pressure: barometric pressure

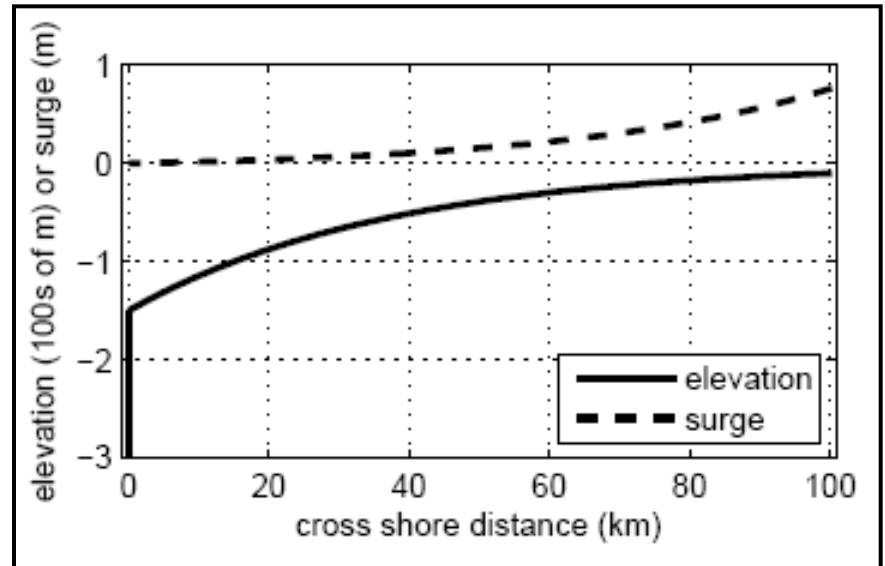
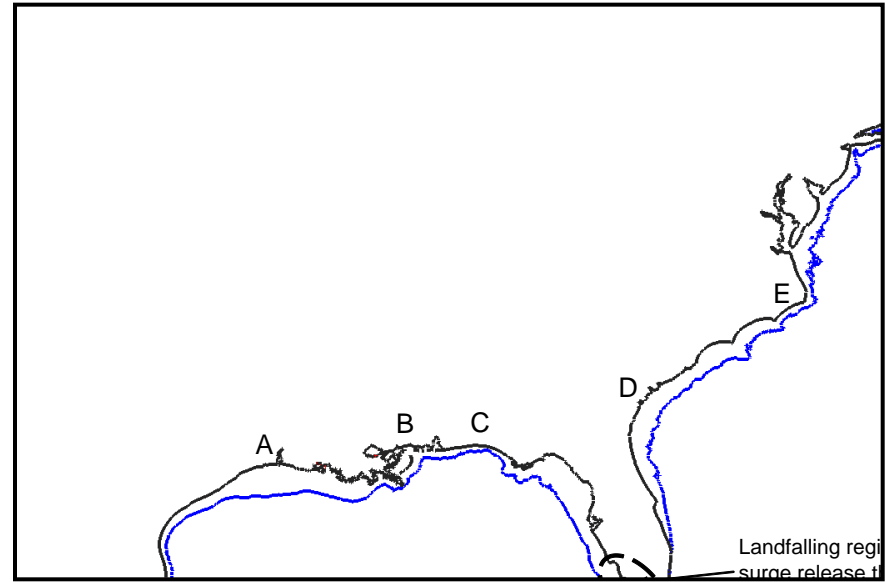
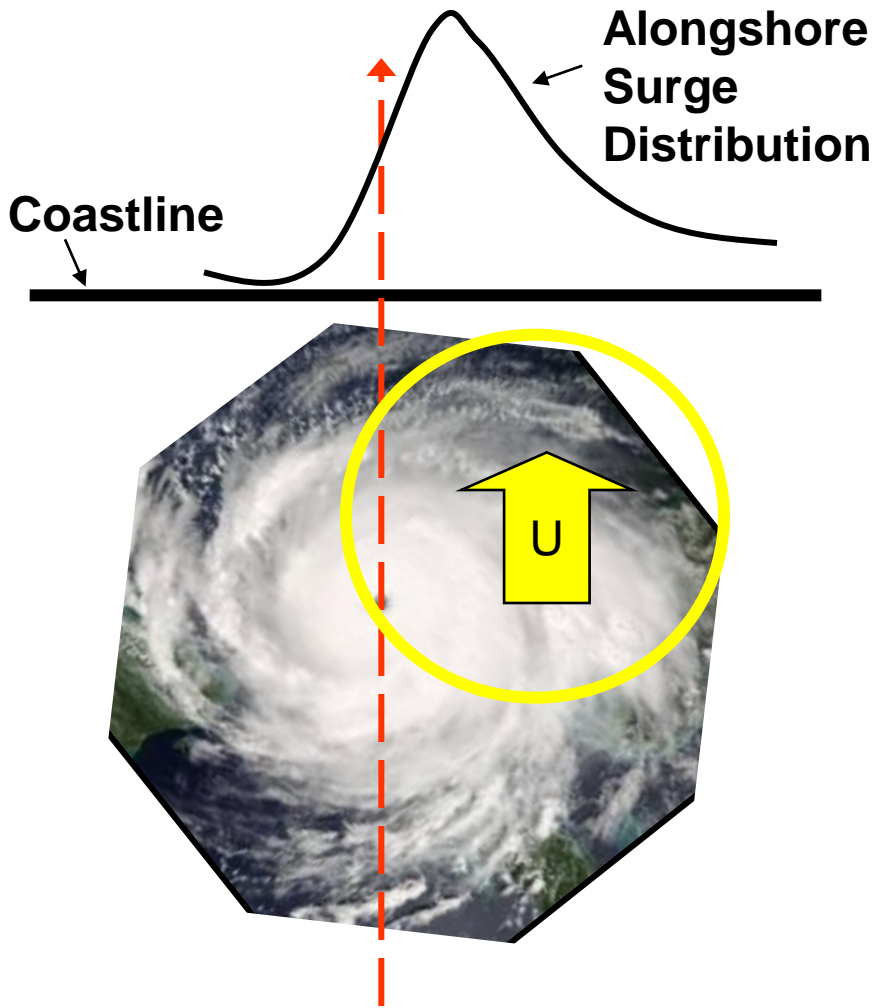


- Wave setup:



Surge Response Functions

Background – Surge Generation



Surge Response Functions

Background – Historical Approach

- Form data set of “largest” storms (measurements or hindcasts)
- Typical applications:
 - Points over Threshold (POT)
 - Annual series
- PARAMETRIC (GEV, Weibull, Log Normal or other assumed form):
 - Considers sampling size effects on “fitted” curve
 - Uses various fitting methods (MLM, MOM, etc.)
 - Allows parametric estimation of return periods larger than given by the historical record
- NON-PARAMETRIC (e.g., EST):
 - No assumptions on data’s probability distribution in interior
 - Uses data to develop distribution in interior
 - Still extrapolates beyond data range using parametric “fit” to data
- Results extremely sensitive to record length
- Storms assumed to be from a homogeneous parent population
 - Climate variability typically excluded

Surge Response Functions

Methodology – Response Function Approach

General form for surge response at location x and time t:

$$\zeta(x, t) = \Phi(\underline{G}, \underline{W} \mid c_p, R_{\max}, v_f, \theta, S(t), t)$$

where

$\zeta(x, t)$ is the storm surge at location x and time t,

Φ is a numerical model used to generate surges over a grid,

\underline{G} is a time invariant grid of bathymetry/topography,

\underline{W} is a wind field over the grid at time t,

c_p is the central pressure,

R_{\max} is the radius to maximum wind speed from the center of the storm,

v_f is the forward velocity of the storm,

θ is the geographic angle of the track, and

$S(t)$ is the position of the storm along the track at time t,

Surge Response Functions

Methodology – Response Function Approach

Joint probability matrix:

$$p(c_p, R_p, v_f, \theta_l, x) = \Lambda_1 \cdot \Lambda_2 \cdot \Lambda_3 \cdot \Lambda_4 \cdot \Lambda_5$$

$$\Lambda_1 = p(c_p | x) = \frac{\partial F[a_0(x), a_1(x)]}{\partial(\Delta p | c_p)} = \frac{\partial}{\partial x} \left\{ \exp \left\{ -\exp \left[-\frac{\Delta p - a_0(x)}{a_1(x)} \right] \right\} \right\} \quad (\text{Gumbel Distribution})$$

$$\Lambda_2 = p(R_p | c_p) = \frac{1}{\sigma(\Delta P)\sqrt{2\pi}} e^{-\frac{(\bar{R}_p(\Delta P) - R_p)^2}{2\sigma^2(\Delta P)}}$$

$$\Lambda_3 = p(v_f | \theta_l) = \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{(\bar{v}_f(\theta_l) - v_f)^2}{2\sigma^2}}$$

$$\Lambda_4 = p(\theta_l | x) = \frac{1}{\sigma(x)\sqrt{2\pi}} e^{-\frac{(\bar{\theta}_l(x) - \theta_l)^2}{2\sigma^2(x)}}$$

$$\Lambda_5 = \Phi(x)$$

Uncertainty:

$$\sigma_{total}^2 = \sigma_{tide}^2 + \sigma_{model}^2 + \sigma_B^2 + \sigma_{waves}^2 + \sigma_{winds}^2 + \sigma_{residual}^2$$

Surge Response Functions

Methodology – Numerical Simulation

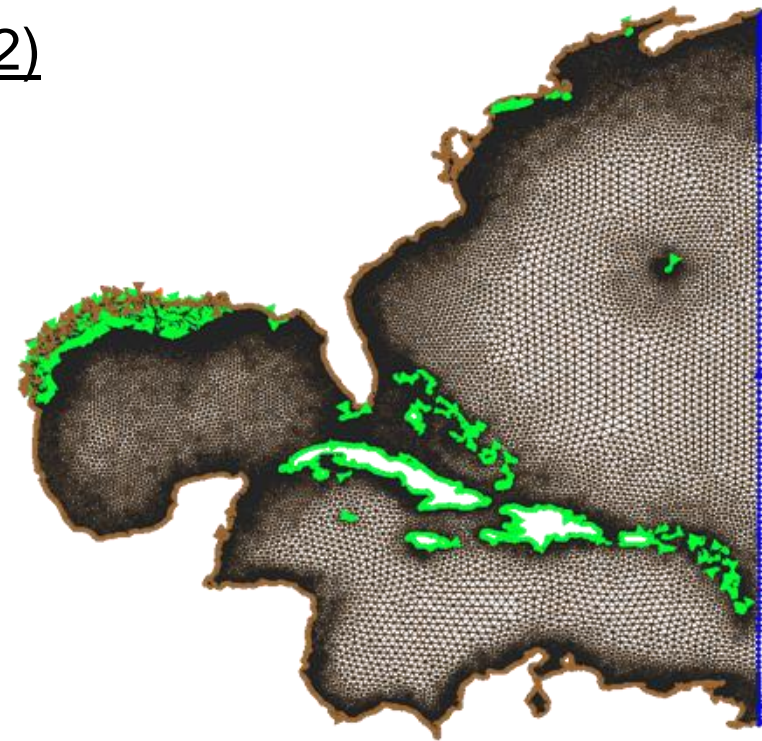
Storm surge – ADCIRC (Luettich *et al.* 1992)

- Hydrodynamic model:

$$\frac{\partial \vec{U}}{\partial t} + (\vec{U} \cdot \nabla_H) \vec{U} = -g \nabla_H \left(\zeta + \frac{p}{g \rho_w} - \alpha \eta \right) + f \vec{k} \times \vec{U} + \frac{\vec{\tau}_s}{H \rho_w} - \frac{\vec{\tau}_b}{H \rho_w}$$

$$\frac{\partial H}{\partial t} + \nabla_H (\vec{U} H) = 0$$

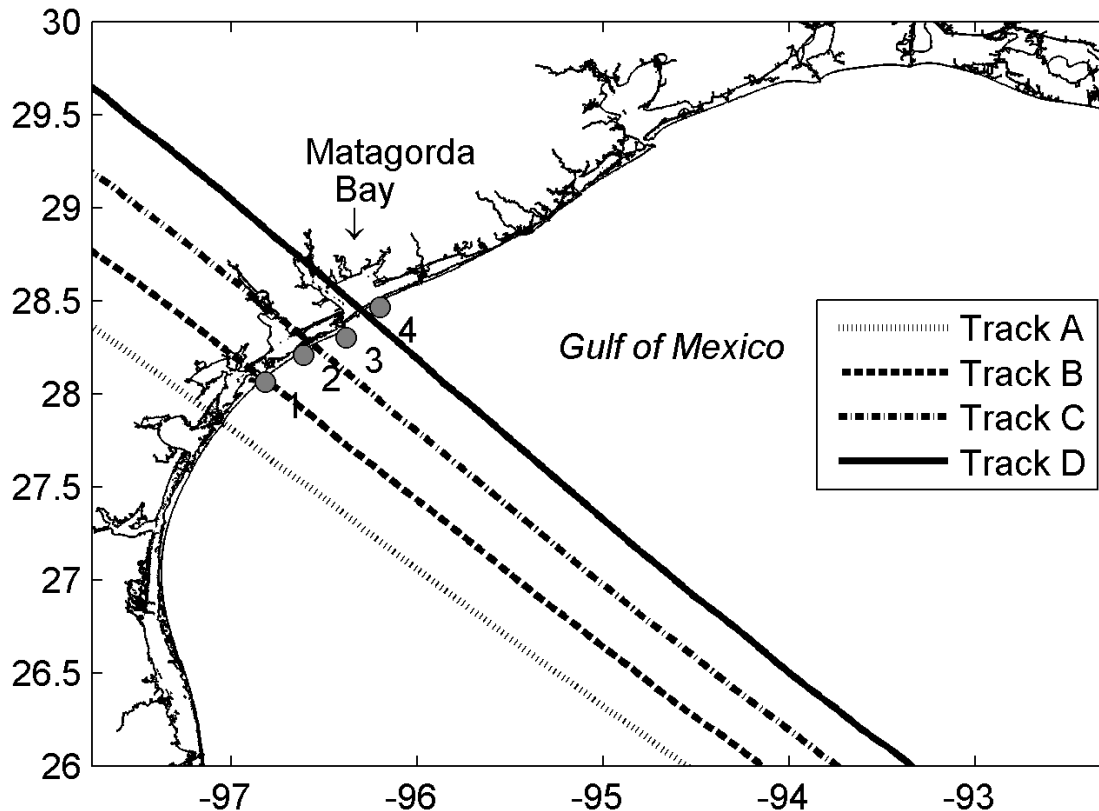
- Finite element, variable resolution
- Model forcing:
 - Wind stress
 - Barometric pressure



Surge Response Functions

Methodology – Numerical Simulation

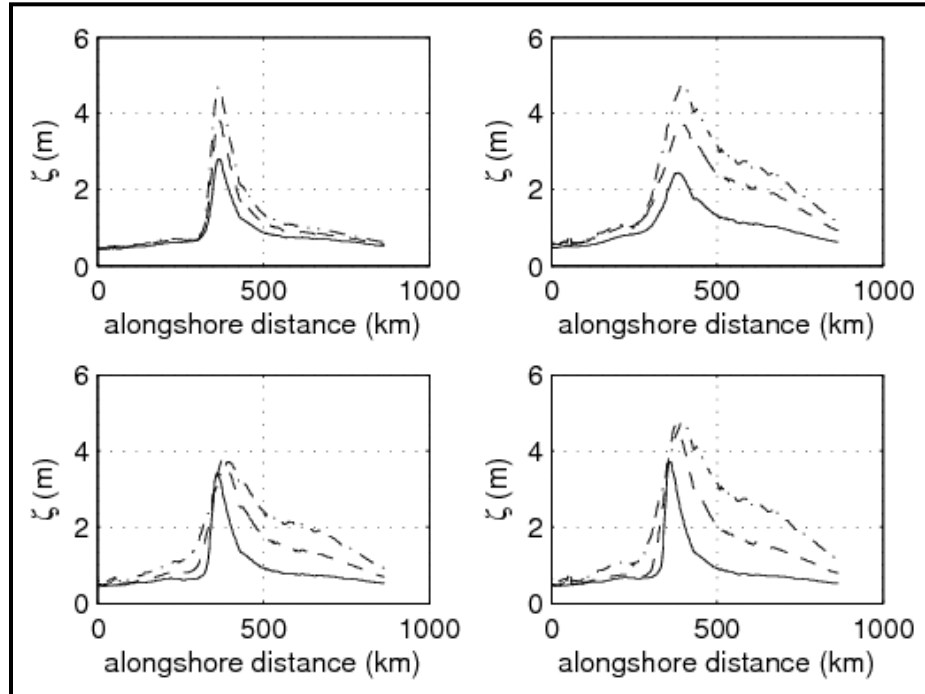
- Planetary Boundary Layer Model (Thompson & Cardone 1996):
 - Input V_f , θ , cp , R_p , track position, ...
 - 75 storms on 4 tracks (V_f constant, $\theta \sim$ constant)



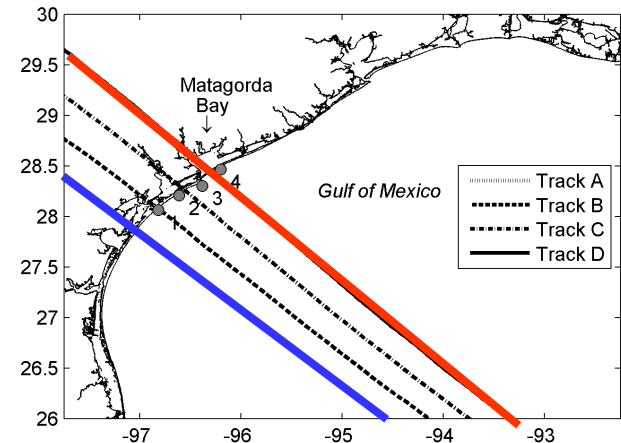
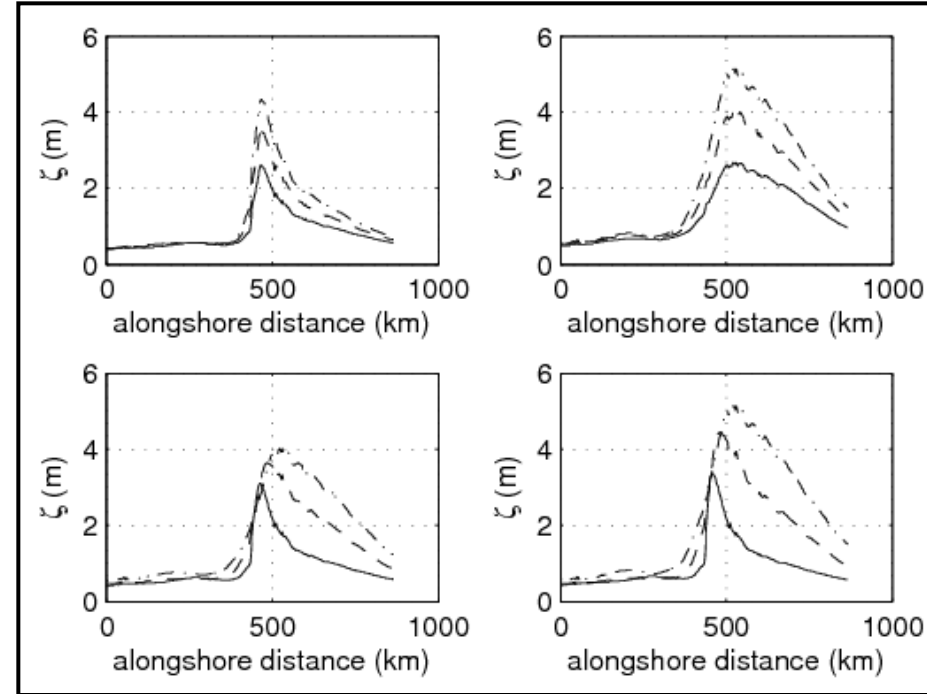
Surge Response Functions

Surge Characteristics – Alongshore Variation

Track A



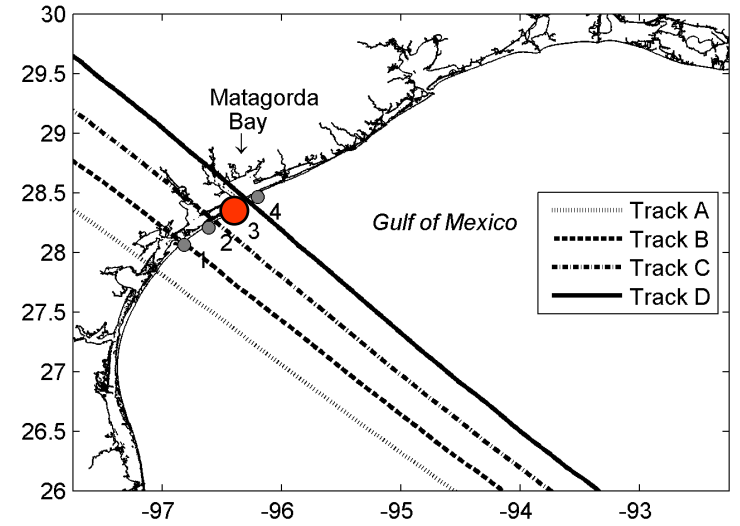
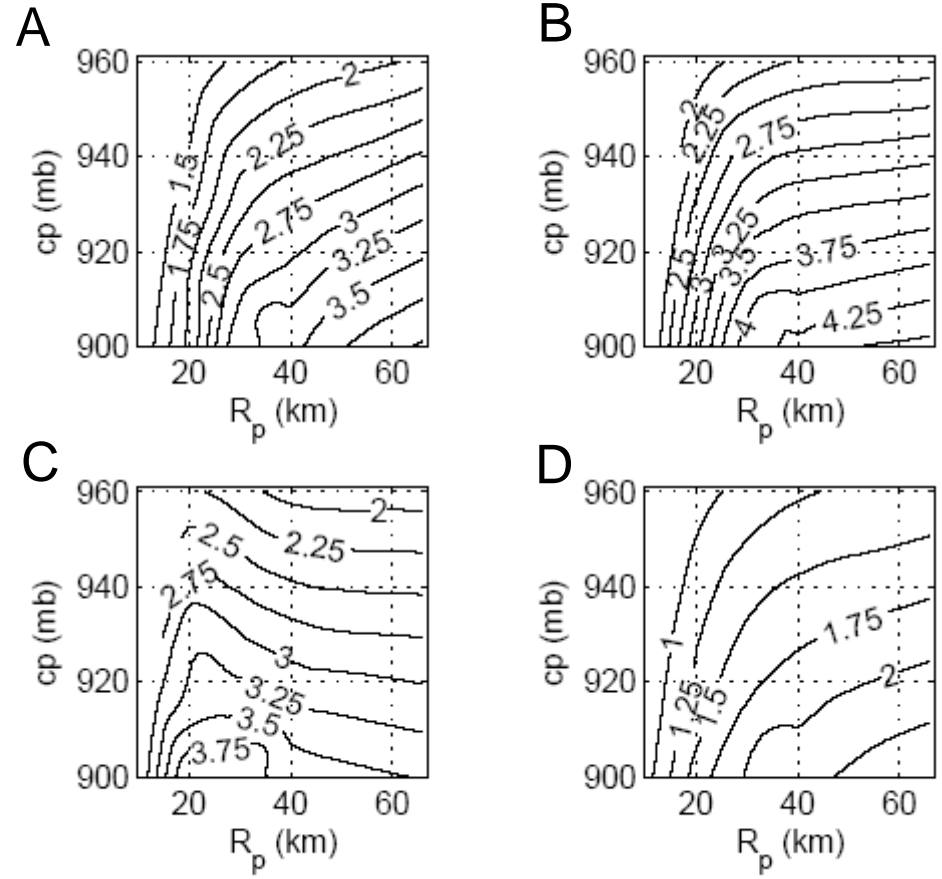
Track D



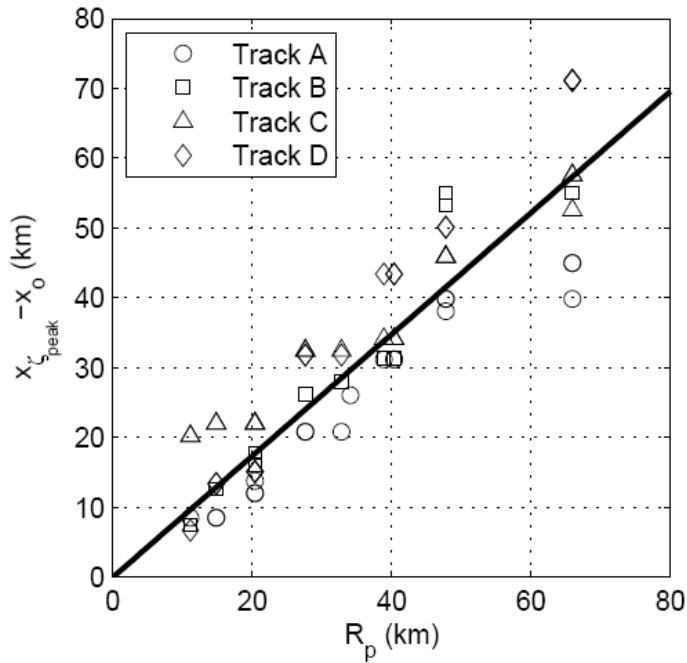
Surge Response Functions

Surge Characteristics – Response Surfaces

Location 3

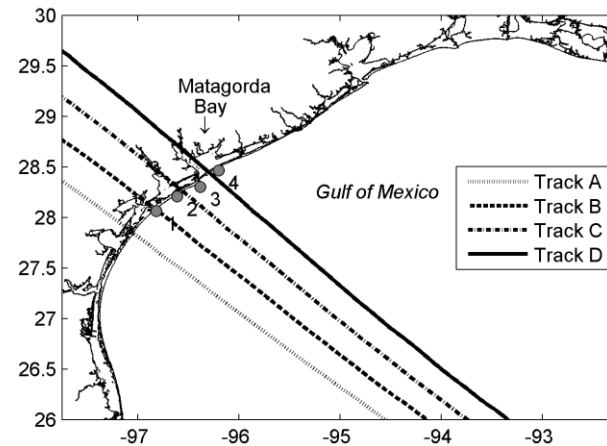
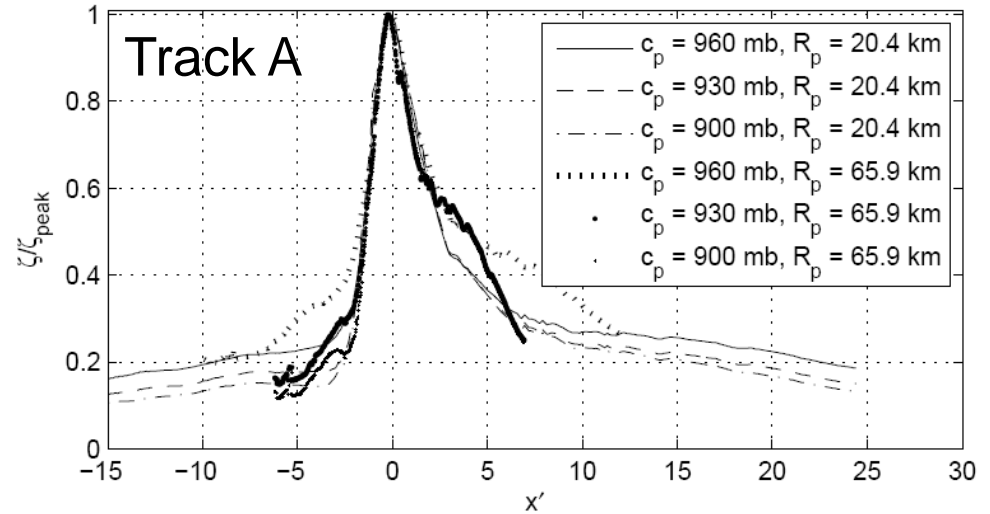


Surge Response Functions Parameterization



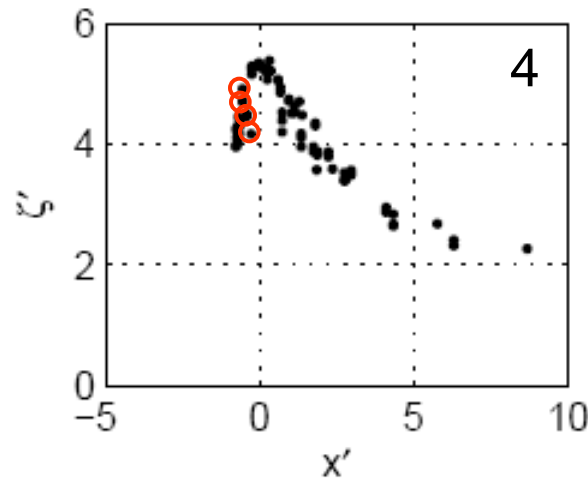
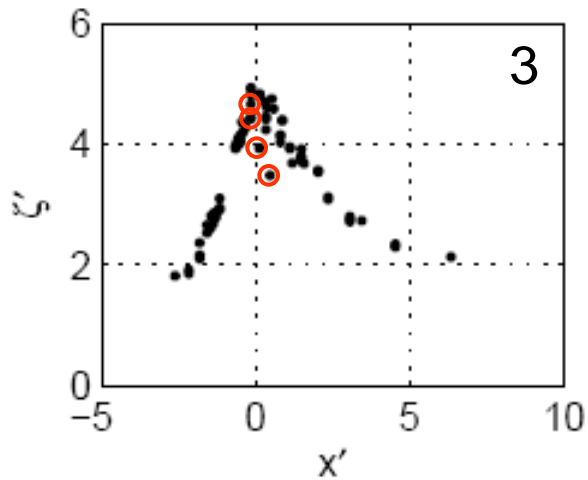
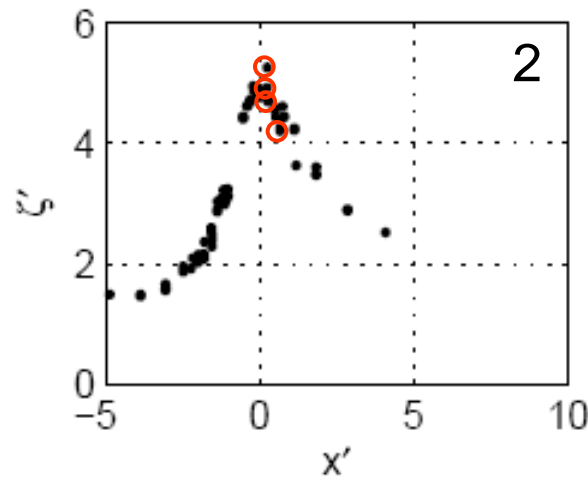
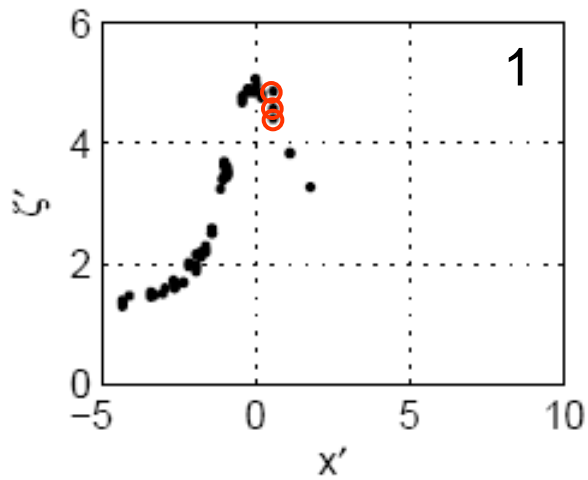
$$x' = \frac{(x - x_0)}{R_p} - \lambda$$

$$\zeta' = \frac{\gamma \zeta}{\Delta p} + m_x \Delta p$$



Surge Response Functions

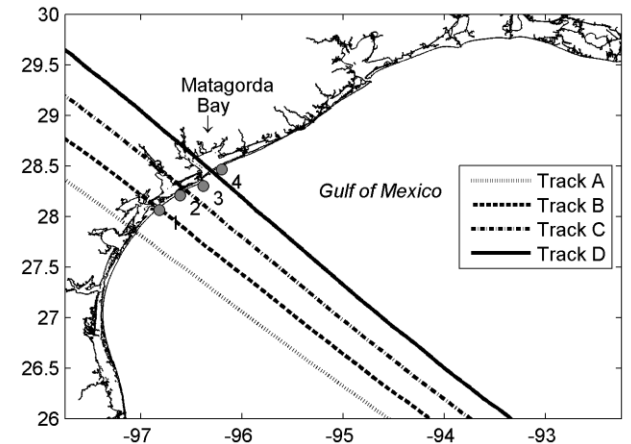
Parameterization – Response Function



$$x'_2 = x' - F(1-R')H(1-R')$$

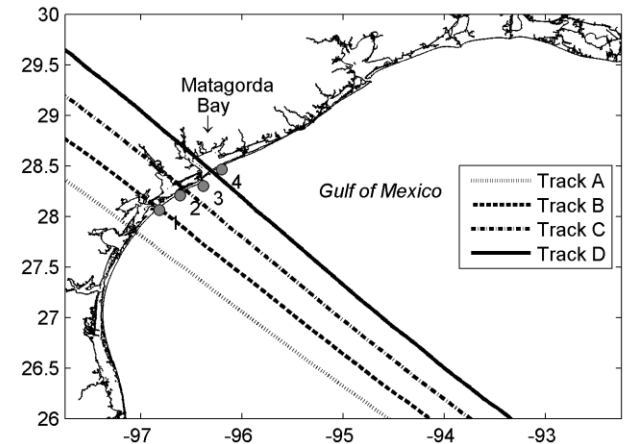
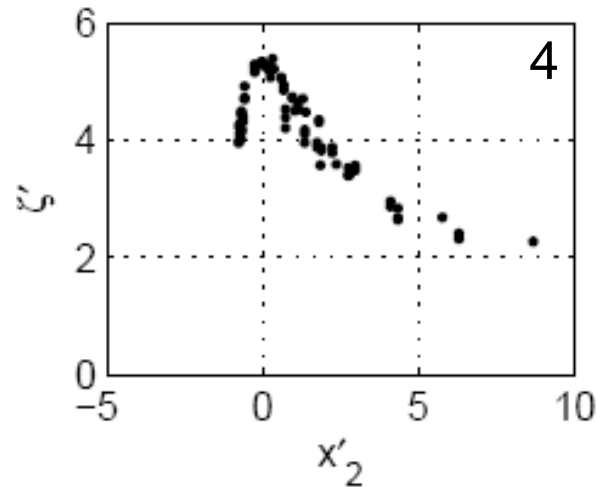
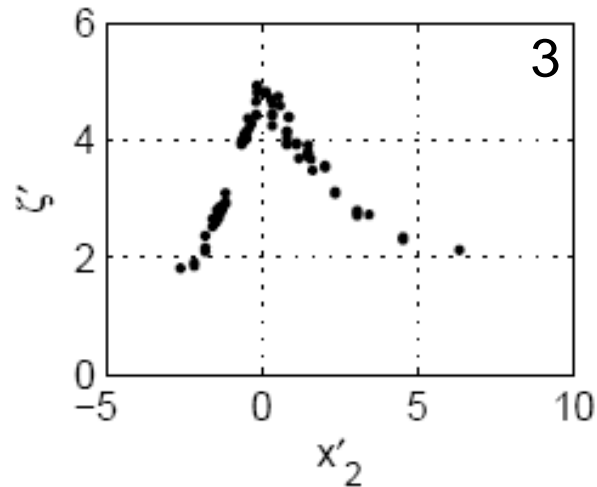
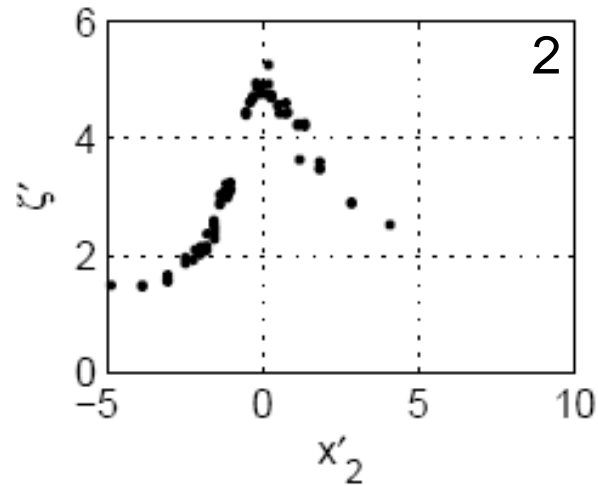
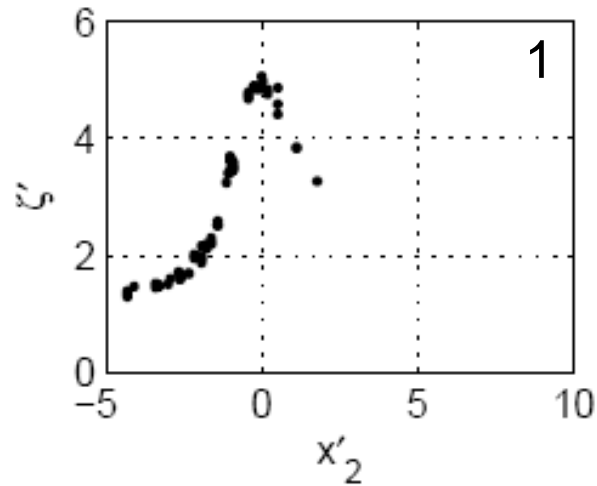
$$R' = R_p/R_{thres}$$

$$F(1-R') = \begin{cases} a_1(1-R') + b_1 & -\lambda \leq x' \leq 0 \\ a_2(1-R') + b_2 & 0 < x' \leq \lambda \\ 0 & \lambda < |x'| \end{cases}$$



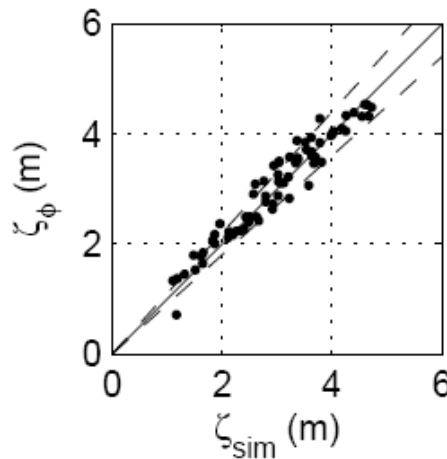
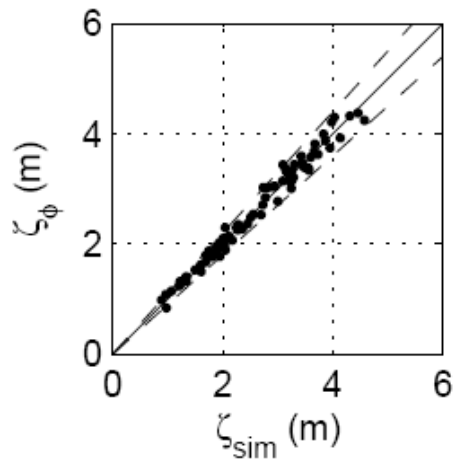
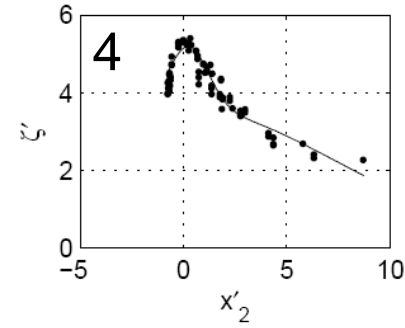
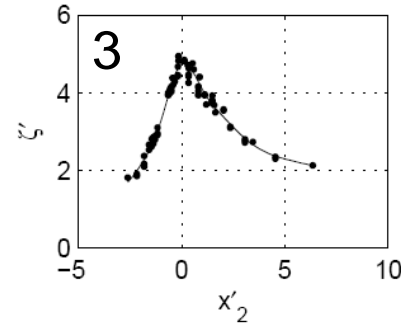
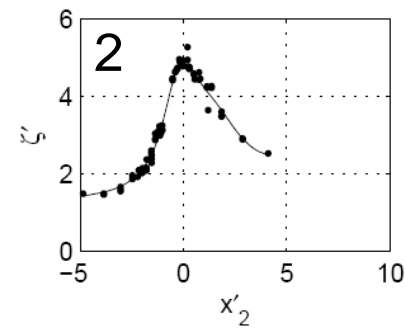
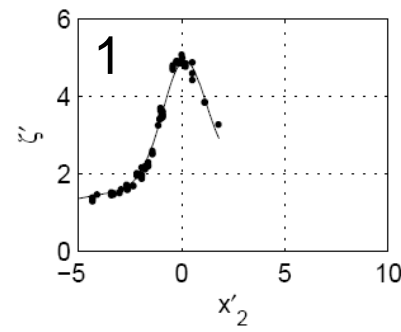
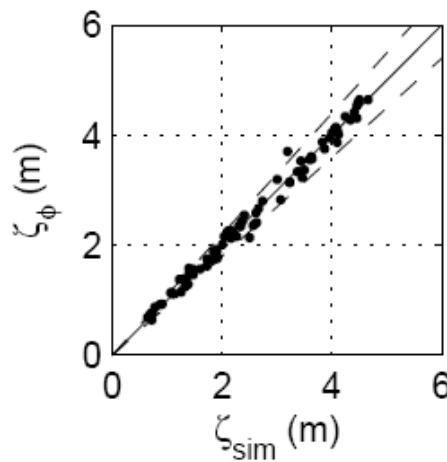
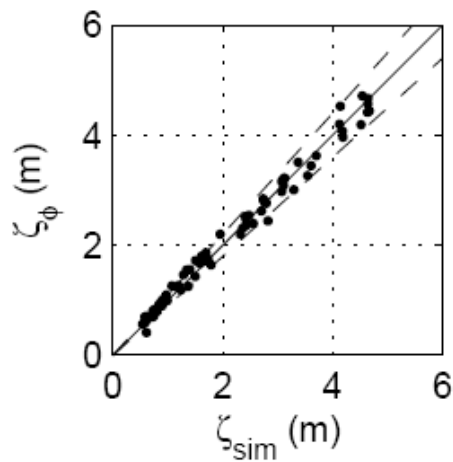
Surge Response Functions

Parameterization – Response Function



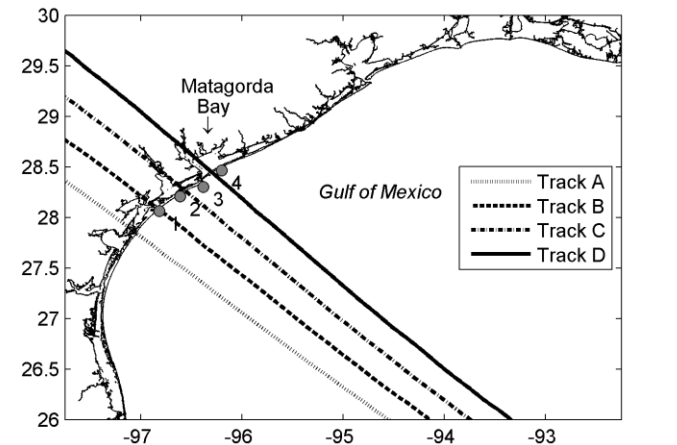
Surge Response Functions

Results – All Four Tracks at 30 km Spacing



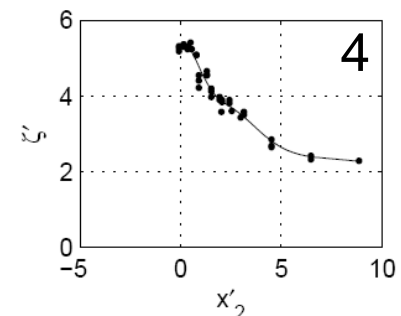
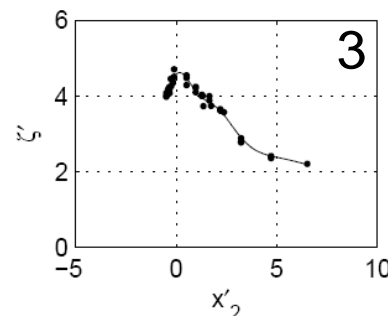
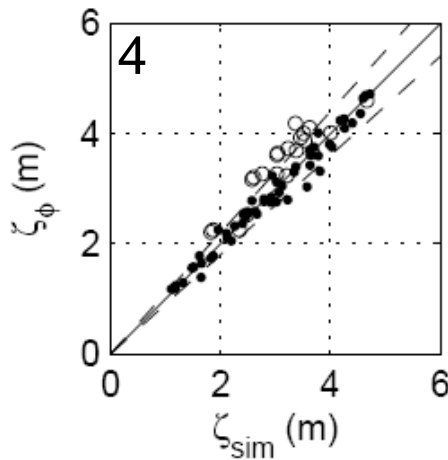
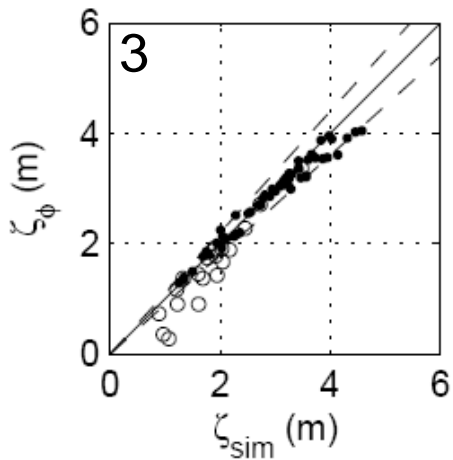
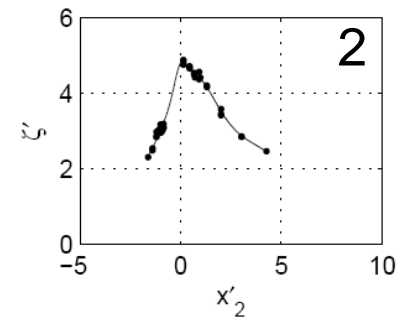
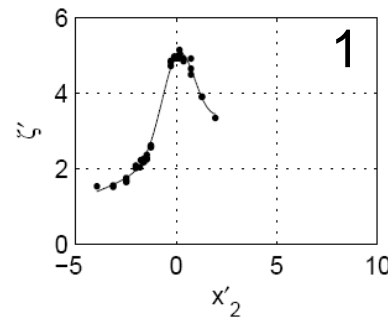
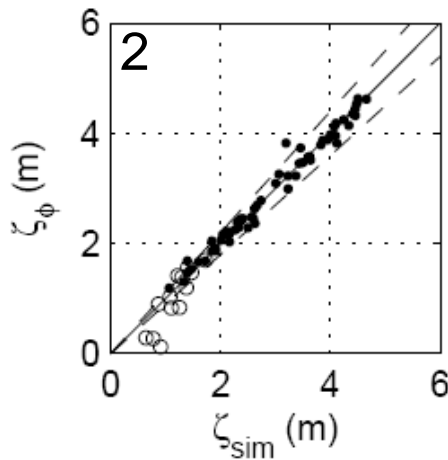
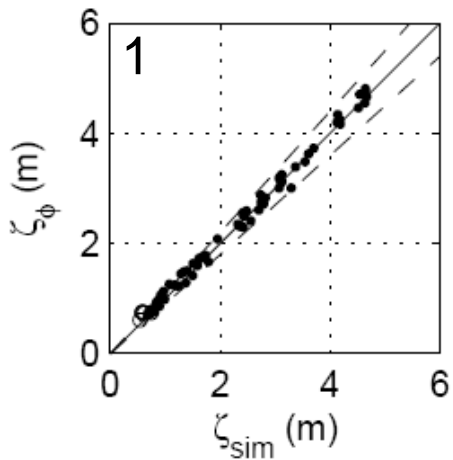
75 simulations:

mean error = 0 – +4 cm, RMS error = 12 – 24 cm



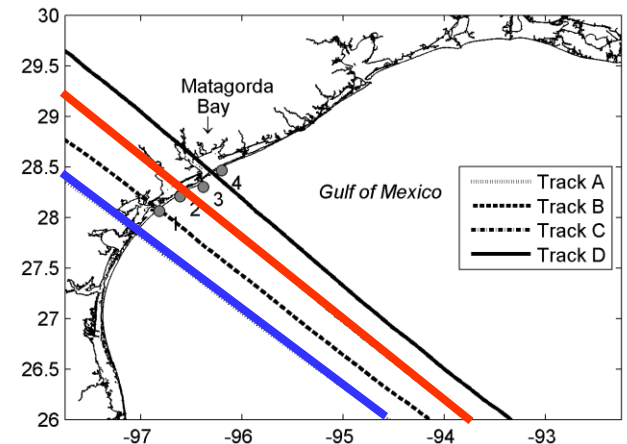
Surge Response Functions

Results – Two Tracks at 60 km Spacing



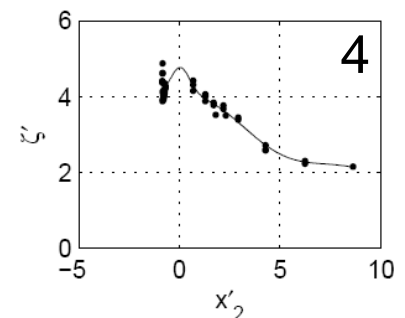
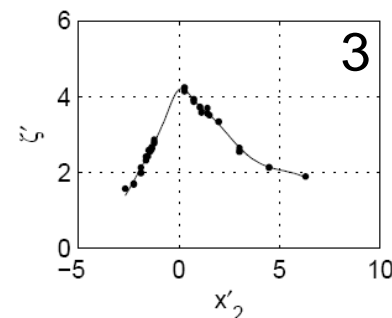
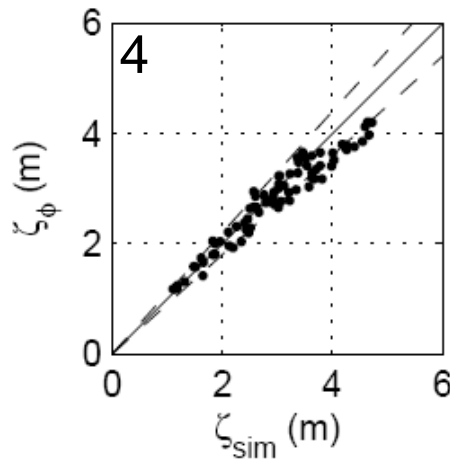
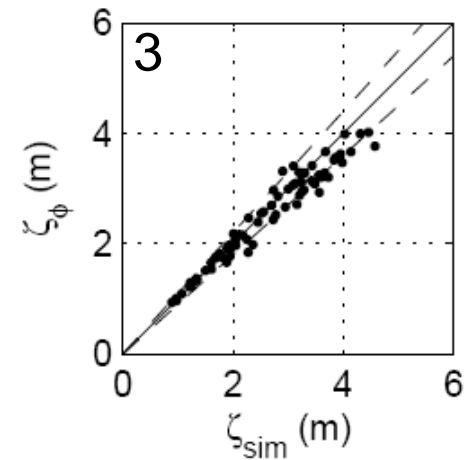
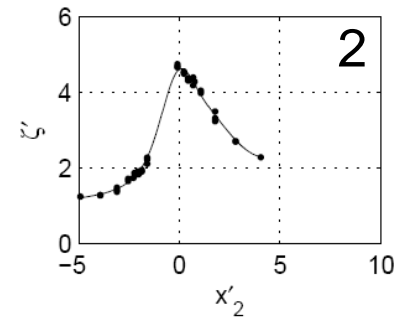
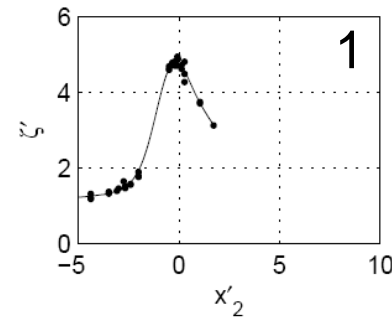
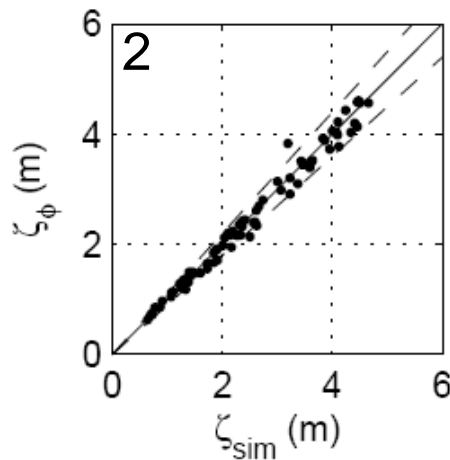
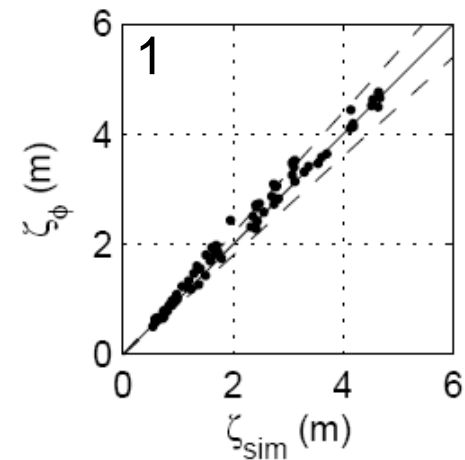
37 simulations:

mean error = -9 – +4 cm, RMS error = 10 – 19 cm



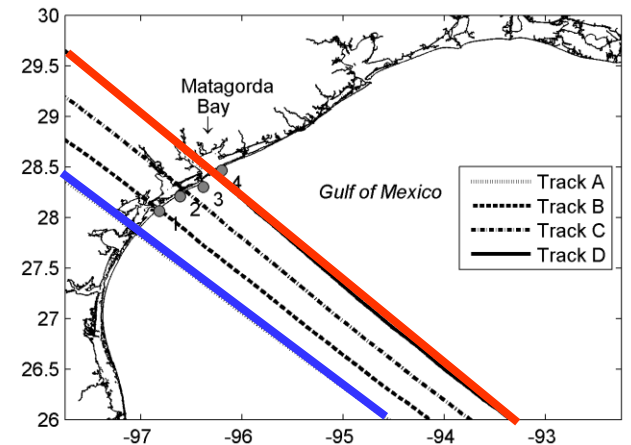
Surge Response Functions

Results – Two Tracks at 90 km Spacing



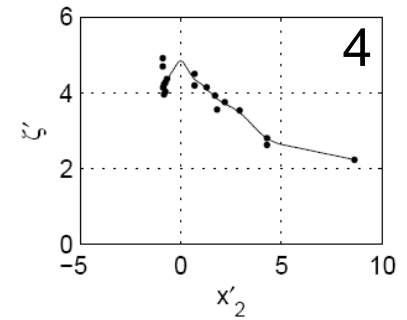
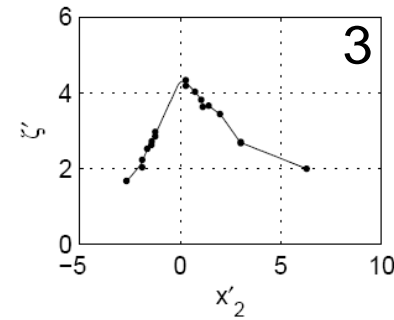
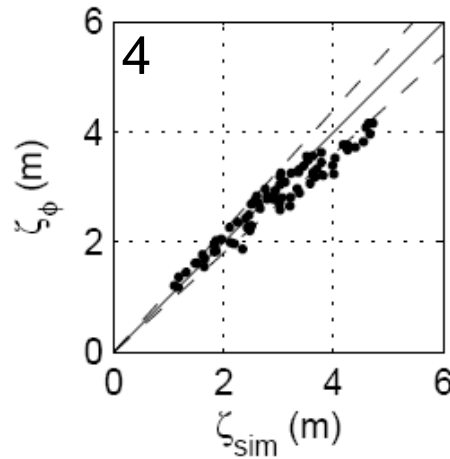
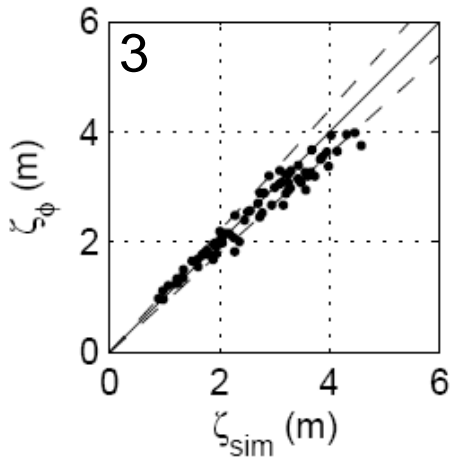
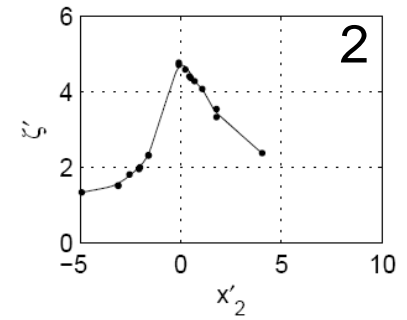
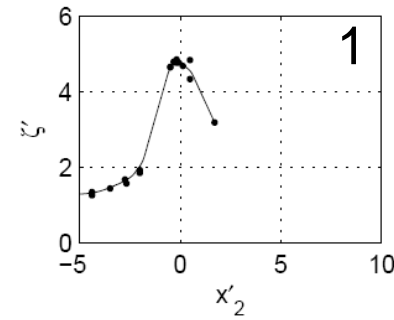
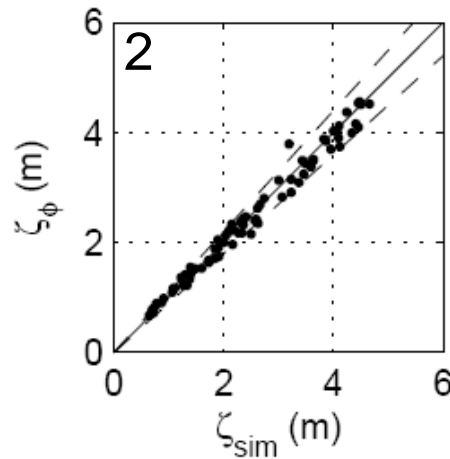
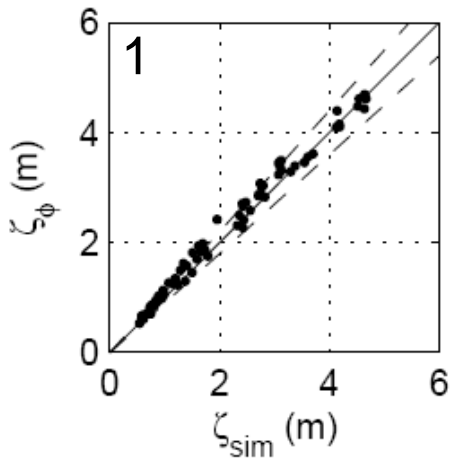
38 simulations:

mean error = -16 – +9 cm, RMS error = 15 – 30 cm



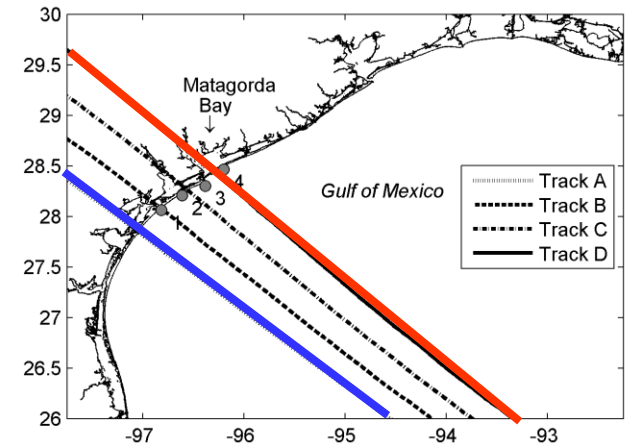
Surge Response Functions

Results – Two Tracks at 90 km Spacing, Limited Storms



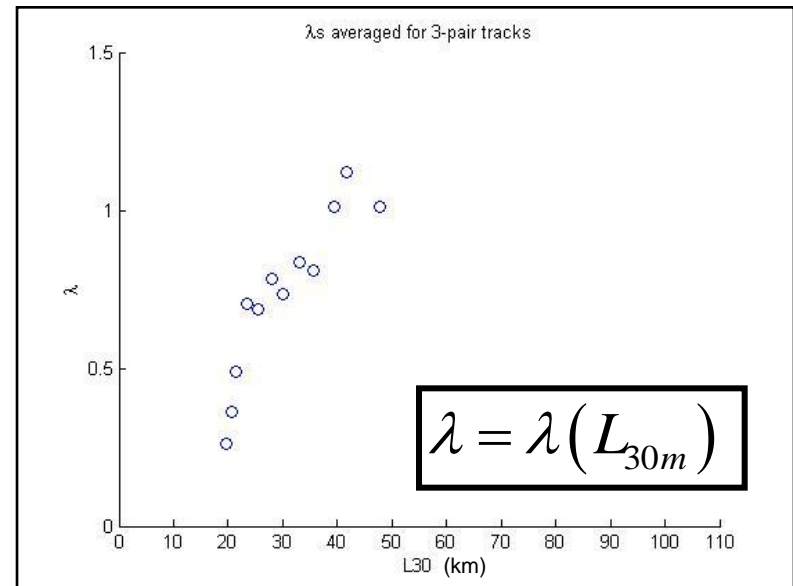
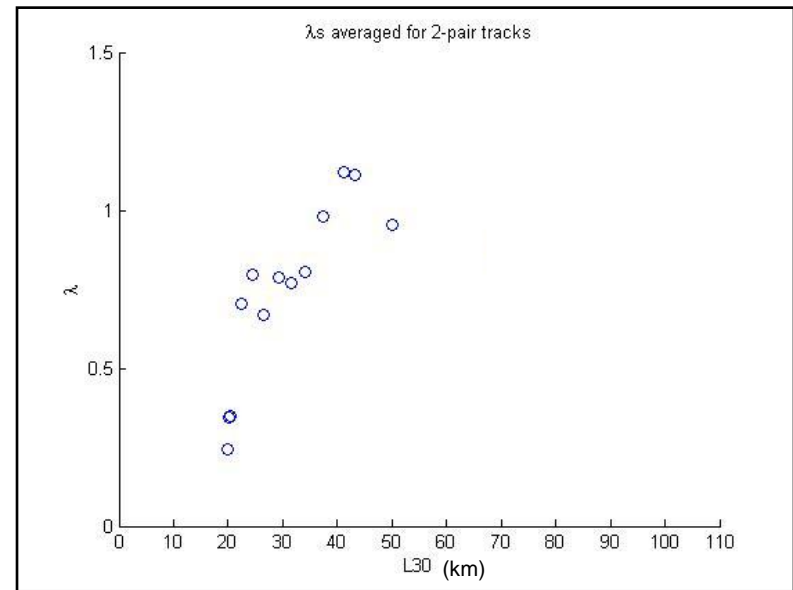
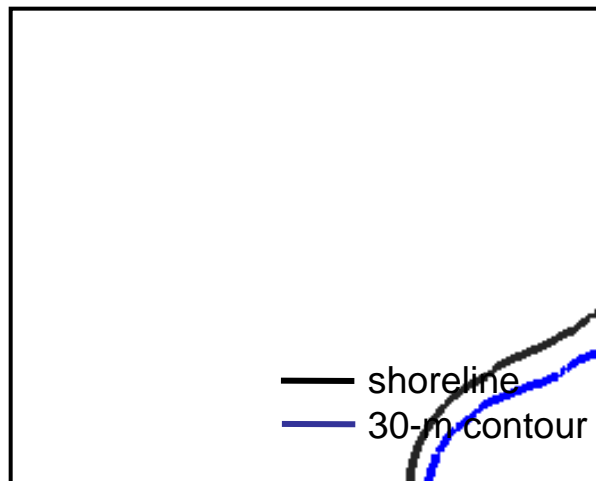
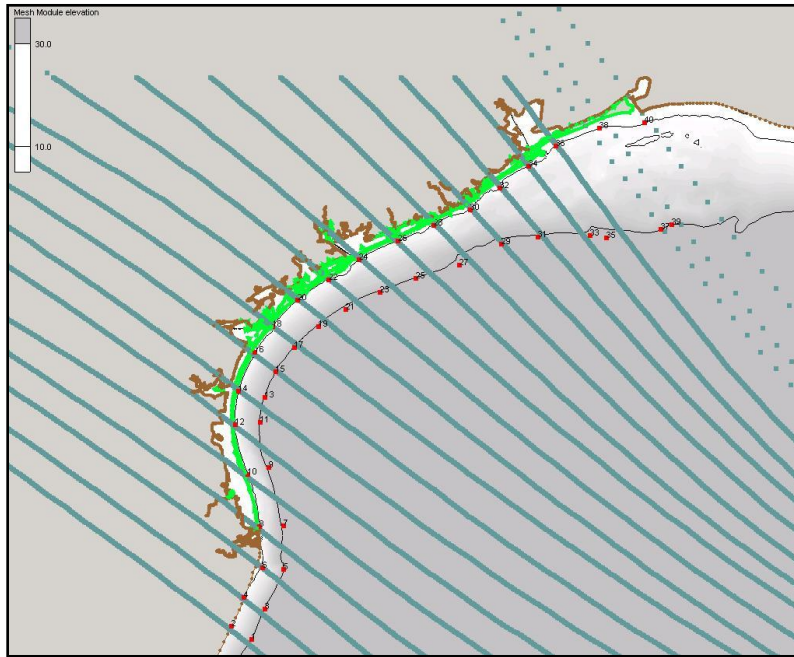
18 simulations:

mean error = -17 – +10 cm, RMS error = 16 – 32 cm



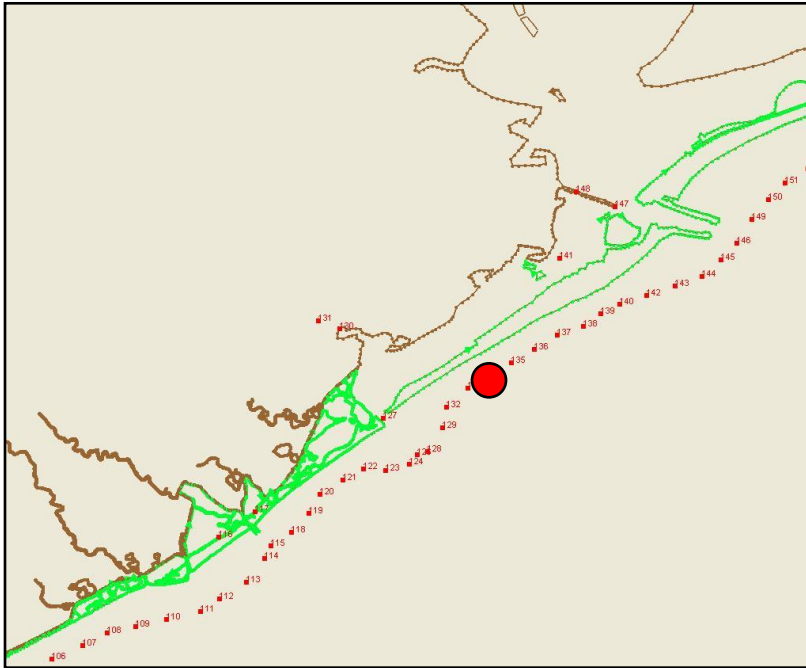
Surge Response Functions

Ongoing Research – Continental Shelf Width (Preliminary)

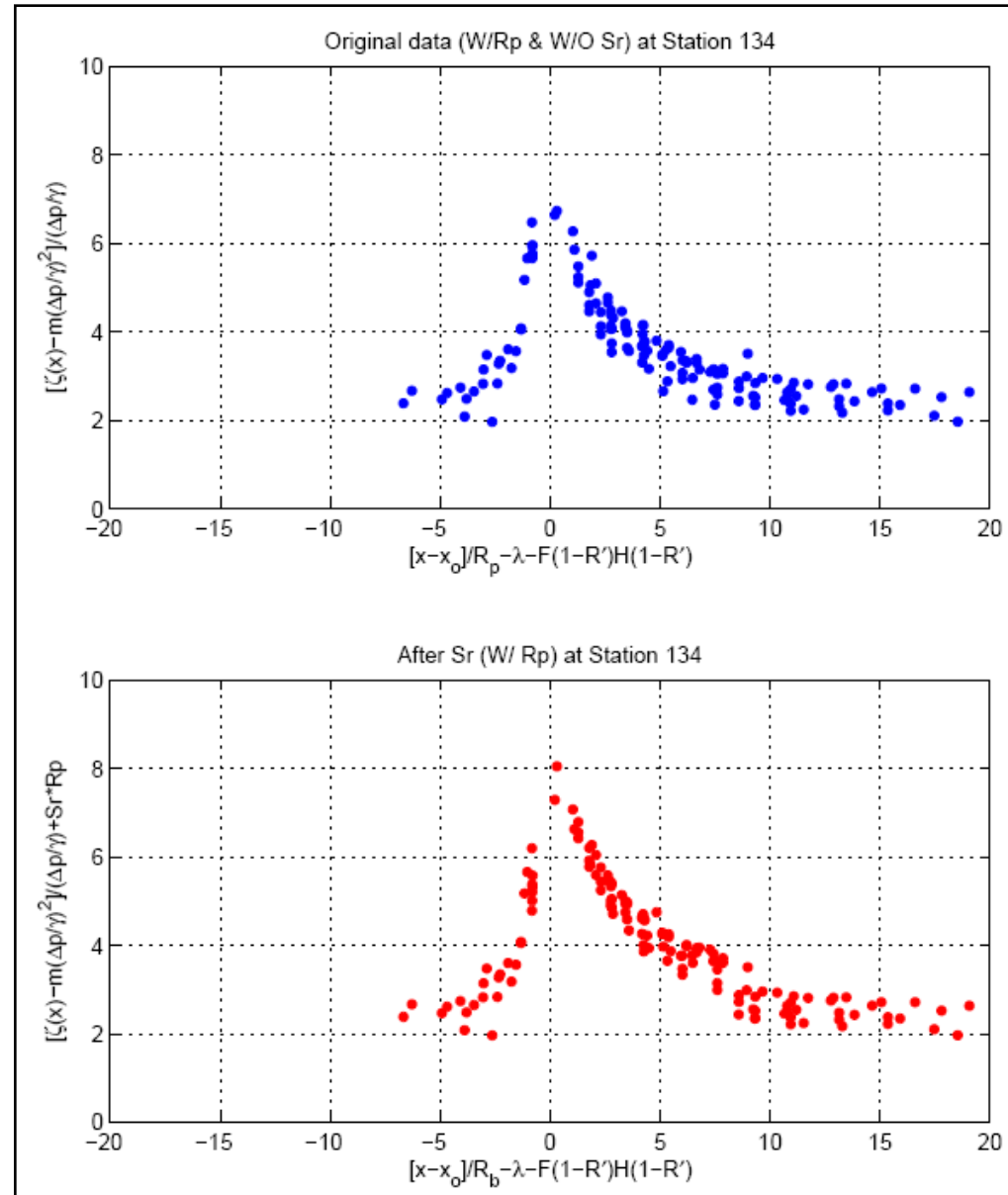


Surge Response Functions

Ongoing Research – Surge and Storm Size (Preliminary)



$$\zeta'_2 = \frac{\gamma \zeta}{\Delta p} + m_x \Delta p + S_R R_p$$



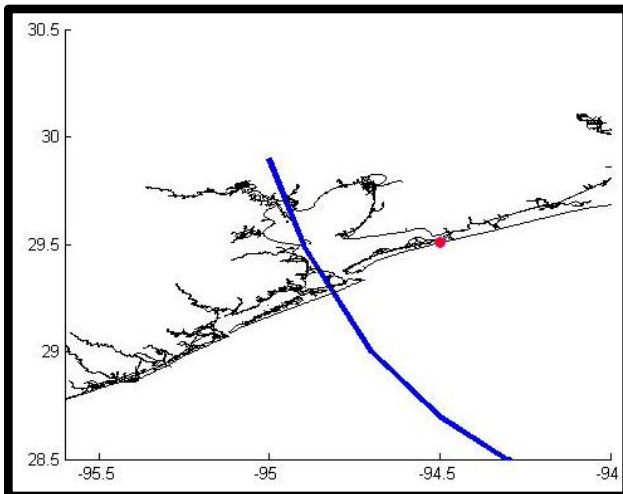
Surge Response Functions

Hurricane Ike – Preliminary Results

Maximum Surge Calculation near Rollover Pass



Rmax[km]	Peak [km]
10	10.78
14	12.48
18	13.32
22	13.88
26	14.29
30	13.76
34	13.30
38	12.94
42	12.65
46	12.41
50	12.21
54	12.04

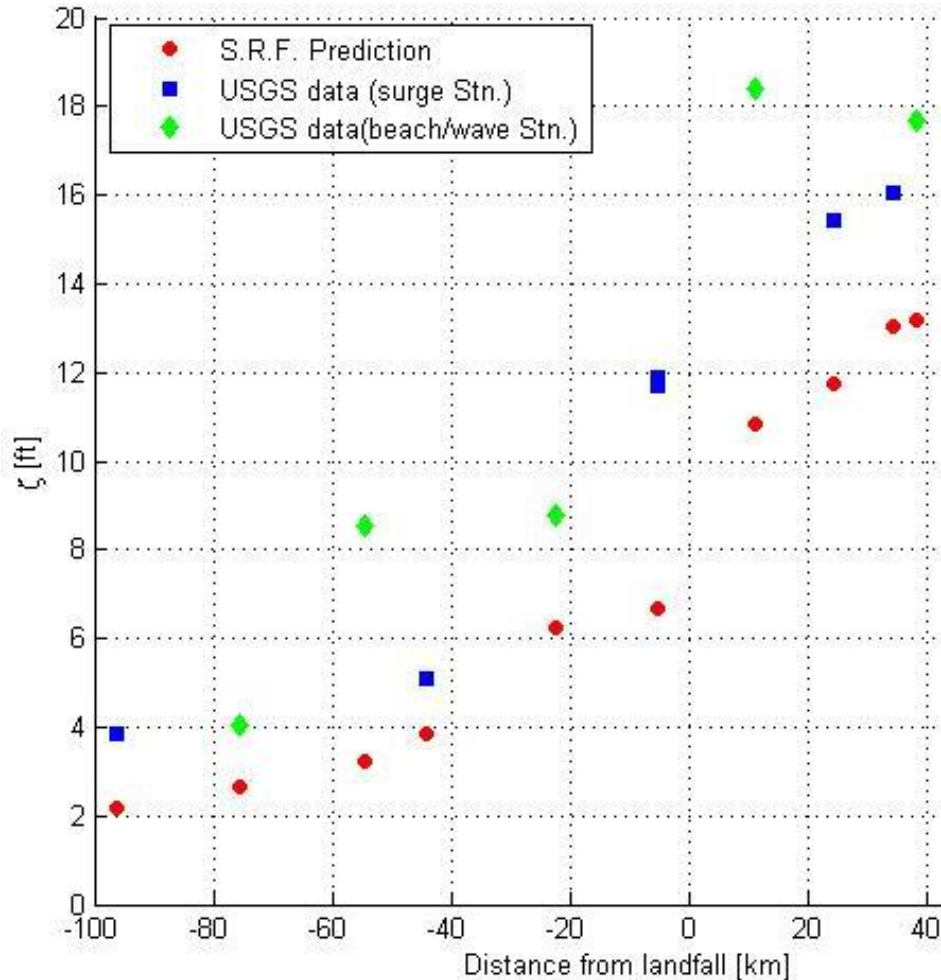


- Hurricane Ike characteristics: $c_p=952$ mb, $R_{max} = 38$ km
- Location 28 km to the right of the landfall
- *Water level elevation by tides and wave setup not included*
- *Impact of barrier island morphology not considered*

FEMA HWM = 14.70 ft, MSL (“wave runup”)

Surge Response Functions Hurricane Ike – Preliminary Results

Comparison to USGS water level gauge data



- Water level elevation by tides and wave setup not included
- Impact of barrier island morphology not considered

ADCIRC Job Characterization on HYDRA

Each ADCIRC simulation ~ 1400 computational hours (32/64 processors)

Each coupled ADCIRC/wave simulation ~ 3500 computational hours (32/64 processors)

Advantages of using Hydra:

- Capable of running nine parallel simulations simultaneously
- Linkage to large data storage via K2 server

Hydra Usage Information for FY09:

- 296 jobs, 146267 cpu hours

Job Type	Total Jobs	Total Cpu Hours	Average Execution Time
1-cpu	153	65	25 minutes
32-cpu	82	76421	32 hours
64-cpu	60	68555	24 hours
128-cpu	1	1224	18 hours

Surge Response Functions Summary

- Surge response approach presents solution to extreme-value statistics for coastal flooding
- Definable characteristics of response surfaces – given a single track:
 - Surge distribution scales with R_p and c_p
- Overall methodology must include a means to reflect uncertainty in predicted response surfaces
- Response surface prediction has potential to extend applicability of limited observation set (i.e. surges in stronger and weaker storms can be estimated)
- Response surface prediction reduces numerical simulation requirements by allowing functional interpolation between simulation results
- Application in coast bays viable